# Design and simulation of half adder and half subtractor using lithium niobate-based waveguide 

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#### Abstract

Half adder and half subtractor are at the core of all arithmetic operations; these optical circuits add or subtract two input bits at a time to produce sum and carry or difference and borrow as outputs, respectively. In this work, Half adder/subtractor design based on the electro-optic principle is proposed. The operating speed of the proposed design is very fast as compared to its electronic counterpart. The design consists of a Mach-Zehnder interferometer as an optical switching device. Performance parameters like extinction ratio, contrast ratio, amplitude modulation, and insertion loss have been computed and obtained as $38.34 \mathrm{~dB}, 31.87 \mathrm{~dB}, 0.16 \mathrm{~dB}$, and 0.025 dB , respectively for the proposed device.


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## 1. Introduction

Electronic digital systems have limited speed and capacity to handle extensive data; to mitigate the limitation, optical technology is the right choice. Optical systems provide large bandwidth along with high data rate [1]-[5]. Optical signal processing is the new research area that offers optical computing, data processing, and ultrafast switching [6], [7]. Researchers have proposed many next-generation optical systems to utilize the great potential of optical computation [7]. Optical waveguides are the critical element to design optical devices and circuits [8]. Till now, many optical devices like logic gates [9]-[12], code converters [13], decoders [14], [15], encoders [16], shift registers [17], [18], counters [19], flipflop [20], [21], optical memories [22], [23], and other combinational, sequential systems have been proposed [24], [25]. Some techniques to implement various logic circuits using cross gain modulation effect in semiconductor optical amplifier (SOA) [26], cross-phase modulation in single SOA based Mach-Zehnder interferometer (MZI) [27], quantum dot semiconductor optical amplifier (QD-SOA) MZI [28], bit differential delay technique with Terahertz Optical Asymmetric Demultiplexers (TOAD) [29], nonlinear material based intensity encoded, semiconductor optical amplifier (SOA)assisted Sagnac switch technology [30], [31], and microring resonator based design [32] are good but have limitations. Cross gain and cross-phase effect in SOA is having the limitation of speed due to the saturation effect of SOA. Bit differential delay techniques are having round trip delay, which increases the time-of-flight (TOF) latency [30], [31], [33]-[36]. A half adder and subtractor
device are implemented in this work using lithium niobatebased MZI (LN-MZI). LN-MZI is a promising solution because of its characteristic features like compact size, thermal stability, integration potential, reconfigurability, and low power consumption. Optical adder and subtractor preform addition and subtraction at very high speed, used as basic building block for high-speed optical computing.

In this paper, half adder and half subtractor devices using the electro-optic effect in lithium niobate MZI have been proposed. Section 2 consists of the working principle of the MZI switch and a mathematical description. Section 3 explains the optical simulation of half adder and subtractor using MZI. Results and discussion are given in section 4. Finally, Section 5 concludes the proposed work.

## 2. Mech-Zehnder interferometer based optical switch

The Mach-Zehnder interferometer (MZI) consists of two 3 dB couplers, is designed using lithium niobate material. Lithium niobate has high electro-optic coefficient (Pockels' coefficient [37], [38]) $30.8 \times 10^{-12} \mathrm{~m} / \mathrm{V}$ and the extraordinary refractive index of 2.191 . MZI is a $2 \times 2$ optical switch. A continuous-wave optical signal of 1330 nm is applied at the first input port of the MZI. The incoming signal's power is divided equally among both waveguides because the coupling coefficient is 0.5 . This signal is controlled by applying an electric voltage $(V)$ at the middle electrode of the MZI. When $V=0$, then the optical signal is obtained at output port OUT2 and $V=6.75 \mathrm{~V}$ then signal appears at output port OUT1 (shown in Fig. 1 (c). Table 1 shows the optical properties of the signal used for the proposed device.

Table 1. Properties of the optical signal

| Parameter | Details |
| :--- | :--- |
| Power | 1 mW |
| Wavelength | 1330 nm |
| Polarization | No applied |
| Optical Signal | Continuous-wave |


(a)

(b)

(c)

Fig. 1. (a) Schematic view of single MZI (b) Output power at port 1 and port 2 (for zero electrode potential, $V=0$ )
(c) Optical switching process (color online)

Fraction $k_{c d}$ (coupling coefficient between 3 dB coupler and output waveguide) transmit build-up signal to output port 2. The material's refractive index can be changed by applying the electric field across it (Pockel's effect). The phenomenon of changing of refractive index by an applied electric field is called the electro-optic effect; the change in the refractive index occurs. Due to this phase changes in an applied electric field. A 1 mW continuous wave is applied at input port 1 . Here $k_{a b}$ is the field coupling coefficient between the first 3 dB coupler and input waveguide, $k_{c d}$ is coupling coefficient between the second 3 dB coupler and output waveguide. The attenuation constant is $\alpha$, and insertion loss is $\gamma . E_{\text {in }}$ is the input electric field applied at the first input port of the MZI. The normalized power at output port OUT1 is $P_{1}$ and at output port OUT2 is $P_{2}$. We assume that the field at point $a, b, c$, and $d$ are $E_{t a}, E_{t b}, E_{t c}$ and $E_{t d}$ respectively. From Fig. 1 (a), field $E_{t a}, E_{t b}, E_{t c}$ and $E_{t d}$ could be written as

$$
\begin{gather*}
E_{t a}=(1-\gamma)^{1 / 2}\left[\sqrt{1-k_{a b}}\left(E_{i n}\right)+j \sqrt{k_{a b}}(0)\right]  \tag{1}\\
E_{t b}=(1-\gamma)^{1 / 2}\left[\sqrt{1-k_{a b}}(0)+j \sqrt{k_{a b}}\left(E_{i n}\right)\right]  \tag{2}\\
E_{t c}=E_{t a} e^{-j \varphi_{1}}  \tag{3}\\
E_{t d}=E_{t b} e^{-j \varphi_{2}} \tag{4}
\end{gather*}
$$

The field at output ports 1 and 2 can be written as

$$
\begin{align*}
& \text { OUT1 }=(1-\gamma)^{1 / 2}\left[\sqrt{1-k_{c d}}\left(E_{t c}\right)+j \sqrt{k_{c d}}\left(E_{t d}\right)\right]  \tag{5}\\
& \text { OUT2 }=(1-\gamma)^{1 / 2}\left[j \sqrt{k_{c d}}\left(E_{t c}\right)+\sqrt{1-k_{c d}}\left(E_{t d}\right)\right] \tag{6}
\end{align*}
$$

After solving the above equation, and put the values of the coupling coefficient $k_{a b}=k_{c d}=0.5$. Here insertion loss $\gamma$ is assumed zero. In a simplified manner, the equations are written as:

$$
\begin{align*}
& \text { OUT1 }=j e^{-j \varphi_{0}} \sin \left(\frac{\Delta \varphi}{2}\right)\left(E_{\text {in }}\right)  \tag{7}\\
& \text { OUT2 }=j e^{-j \varphi_{0}} \cos \left(\frac{\Delta \varphi}{2}\right)\left(E_{\text {in }}\right) \tag{8}
\end{align*}
$$

where assumed that $\varphi_{0}=\frac{\varphi_{1}+\varphi_{2}}{2}$ and $\Delta \varphi=\varphi_{1}-\varphi_{2}$
Above equations 7 and 8 are helpful to design MZI as a switch.

## 3. Optical simulation of half adder and subtractor using MZI

Half adder is a combinational circuit having two binary bits (augend and addend) and two binary outputs (sum and carry). It adds two inputs ( $B$ add with $A$ ) and produces the sum ( $S$ ) and carry ( $C$ ). Half subtractor subtracts two binary inputs ( $B$ is subtracted from $A$ ) and produces difference $(D)$ and borrow $(B)$ as output. Table 2 has a truth table of half adder and half subtractor. Fig. 2 shows the schematic diagram of the proposed half adder and subtractor circuit. This circuit can perform addition and subtraction simultaneously. The expression for Carry (C) and Sum ( $S$ ) is $C=A B$ and $S=A \oplus B$ and for difference ( $D$ ) and Borrow ( $B$ ) is $D=A \oplus B$ and $B=\bar{A} B$.

Here input $A$ is applied at the second electrodes of MZI AS1, and input $B$ is applied at MZI AS2, AS3, and AS4, respectively. There is no delay among the inputs, so no additional synchronization is required. Here an optical signal is applied at the first input port of AS1.

Table 2. The truth table of half adder and half subtractor

| Inputs |  | Output of half adder/ Subtractor |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | B | $\left(\frac{S}{D}\right)$ | Power <br> $(\mathrm{mW})$ | $(C)$ | Power <br> $(\mathrm{mW})$ | $(B)$ | Power (mW) |
| Low | Low | Low | 0.0886 | Low | 0.0604 | Low | 0.0675 |
| Low | High | High | 0.9994 | Low | 0.0023 | High | 0.9894 |
| High | Low | High | 0.9997 | low | 0.0038 | Low | 0.0041 |
| High | High | Low | 0.0018 | High | 0.9915 | Low | 0.0065 |



Fig. 2. Schematic diagram of half adder and subtractor circuit

Table 3. Simulation parameters for half adder and half subtractor

| S <br> No. | Parameters | Value(s) |
| :--- | :--- | :--- |
| 1 | $k_{a b}=k_{b a}$ (coupling <br> coefficient input port) | 0.50 |
| 2 | $k_{c d}=k_{d c}$ (coupling <br> coefficient output port) | 0.50 |
| 3 | $\lambda$ operating wavelength |  | $1.30 \mu \mathrm{~m}$.

The proposed structure is simulated using the beam propagation method (BPM) is shown in Fig. 3. The device has four MZIs. An optical signal is provided at the first input port of AS1. The first and second output port of AS1 is connected with the first and second output port of AS3.

The second output port of AS2 is considered as a sum/difference port. Similarly, the first and second output port of MZI AS1 is joined with the second input port of MZI AS4 and the first input port of MZI AS2. The second output of MZI AS4 shows carry (C), and the first output port of the MZI AS2 shows borrow (B).


Fig. 3. BPM layout of half adder and subtractor (color online)

Various combinations of inputs $A$ and $B$ and corresponding outputs carry, sum/difference, and borrow for half adder, and subtractor are obtained using the beam propagation method (shown in Fig. 4). The presence and absence of light signal indicate that the signal is at logic high or a logic low.


Fig. 4. Simulation result of half adder and subtractor using beam propagation method for various inputs ( $A, B=00,01,10,11$ )(color online)

The theoretical results are verified by numerical simulation. The power at output port is written as (using equations 9 and 10);

$$
\begin{gather*}
P_{C}=\left|\left[e^{-j \varphi_{0 A S_{1}}} \sin \left(\frac{\Delta \varphi_{A S 1}}{2}\right) e^{-j \varphi_{0}{ }_{A S 2}} \sin \left(\frac{\Delta \varphi_{A S 2}}{2}\right)\right]\right|\left(E_{\text {in }}\right) \\
P_{\frac{S}{D}}=\left\lvert\,\left[e^{-j \varphi_{0 A S 1}} \sin \left(\frac{\Delta \varphi_{A S 1}}{2}\right) e^{-j \varphi_{0 A S 3}} \cos \left(\frac{\Delta \varphi_{A S 3}}{2}\right)+\right.\right. \\
\left.e^{-j \varphi_{0 A S 1}} \cos \left(\frac{\Delta \varphi_{A S 1}}{2}\right) e^{-j \varphi_{0 A S 3}} \sin \left(\frac{\Delta \varphi_{A S 3}}{2}\right)\right] \mid\left(E_{\text {in }}\right)  \tag{10}\\
P_{B}=\left|\left[e^{-j \varphi_{0 A S 1}} \cos \left(\frac{\Delta \varphi_{A S 1}}{2}\right) e^{-j \varphi_{0 A S 4}} \sin \left(\frac{\Delta \varphi_{A S 4}}{2}\right)\right]\right|\left(E_{\text {in }}\right) \tag{11}
\end{gather*}
$$

where $\varphi_{1 A S i}=\frac{\varphi_{1 i}+\varphi_{1 i}}{2}$ is the phase difference between the two arms of MZI, $E_{i n}$ is the input optical signal. Half adder and half subtractor proposed using QD-SOA requires two additional power sources to pump optical
signals from one port to another. Implementing a simple circuit using QD-SOA requires more components; the complexity of the circuit is increased. In addition, an injection current is also required. In lithium niobate-based MZI, no injection is needed, and able to operate at 160 Gbps . Unlike QD-SOA, different wavelength signals and orthogonally polarized light signals are not required.

## 4. Results and discussion

The performance parameter of the proposed half adder and subtractor device, extinction ratio (ER), contrast ratio (CR), amplitude modulation (AM), insertion loss (IL), and relative eye-opening (Eye), has been computed from the simulated output [39], [40].

$$
\begin{align*}
& \mathrm{ER}(\mathrm{~dB})=10 \log \left(\frac{P_{\text {min }}^{1}}{P_{\text {max }}^{0}}\right)  \tag{12}\\
& \mathrm{CR}(\mathrm{~dB})=10 \log \left(\frac{P_{\text {mean }}^{1}}{P_{\text {mean }}^{0}}\right)  \tag{13}\\
& \mathrm{AM}(\mathrm{~dB})=10 \log \left(\frac{P_{\text {max }}^{1}}{P_{\text {min }}^{0}}\right)  \tag{14}\\
& \mathrm{IL}(\mathrm{~dB})=10 \log \left(\frac{P_{\text {out }}}{P_{\text {in }}}\right)  \tag{15}\\
& \text { Eye }=\left(\frac{P_{\text {min }}^{1}-P_{\text {max }}^{0}}{P_{\text {min }}^{1}}\right) \times 100 \% \tag{16}
\end{align*}
$$

where $P_{\text {max }}^{1}\left(P_{\text {max }}^{0}\right), P_{\text {mean }}^{1}\left(P_{\text {mean }}^{0}\right)$ and $P_{\text {min }}^{1}\left(P_{\text {min }}^{0}\right)$ are the maximum, mean, and minimum values of power at the output for high ' 1 ' (low ' 0 ') levels. $P_{\text {out }}$ and $P_{\text {in }}$ are the power at the output and input port, respectively.

The high value of ER is desirable for switching the optical signal. Fig. 5 is a plot between extinction ratio vs. wavelength, and Fig. 6 depicts the relation between ER and coupling ratio. Max extinction ratio $(38.34 \mathrm{~dB})$ is achieved at $1.3 \mu \mathrm{~m}$. The coupling ratio is taken 0.5 for the device, and maximum ER is obtained at this point.

For proper operation of the device, the contrast ratio should be high as possible so that maximum input power is delivered at the output port. The value of the $C R$ is calculated, and its value found $31.87 \mathrm{~dB}, 28.19 \mathrm{~dB}$, and 30.29 dB (Fig. 7) for carry, sum/difference, and borrow, respectively. The amplitude modulation should be small. Fig. 8 shows a variation of amplitude modulation vs. wavelength.


Fig. 5. Extinction ratio vs. wavelength (color online)


Fig. 6. Extinction ratio vs. coupling ratio (color online)


Fig. 7. Contrast ratio vs. wavelength (color online)


Fig. 8. Amplitude modulation vs. wavelength (color online)


Fig. 9. Insertion loss vs. wavelength (color online)

Table 4. Compared parameters values with the others work

| Parameter | Carry <br> (C) | (S/D) | Borrow <br> (B) | Ref |
| :---: | :---: | :---: | :---: | :---: |
| Extinction ratio (ER) | $\begin{gathered} 16.91 \\ \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 8.77 \\ \mathrm{~dB} \end{gathered}$ | - | [41] |
| Contrast ratio (CR) | $\begin{gathered} 19.73 \\ \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 11.82 \\ \mathrm{~dB} \end{gathered}$ | - |  |
| Amplitude modulation (AM) | $\begin{gathered} 0.09 \\ \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 0.09 \\ \mathrm{~dB} \end{gathered}$ | - |  |
| Insertion loss (IL) | - | - | - |  |
| Eye opening | 97.0\% | 86.7\% | - |  |
| Extinction ratio (ER) | $\begin{gathered} 38.34 \\ \mathrm{~dB} \\ \hline \end{gathered}$ | $\begin{gathered} 35.89 \\ \mathrm{~dB} \\ \hline \end{gathered}$ | 37.04 dB | Proposed |
| Contrast ratio (CR) | $\begin{gathered} 31.87 \\ \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 28.19 \\ \mathrm{~dB} \end{gathered}$ | 30.29 dB |  |
| Amplitude modulation (AM) | $\begin{gathered} 0.16 \\ \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 0.20 \\ \mathrm{~dB} \end{gathered}$ | 0.18 dB |  |
| Insertion loss (IL) | $\begin{gathered} 0.025 \\ \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 0.098 \\ \mathrm{~dB} \\ \hline \end{gathered}$ | 0.081 dB |  |
| Eye opening | 94.7\% | 85\% | 93.1\% |  |

Table 4 consists of the analysis of the comparative parameter of the proposed device. Fig. 10 consists of an eye diagram for the sum/difference of the half adder and subtractor device. The eye-opening for the device is
desirable, and it is obtained $85 \%$ for the sum/difference output port (from Table 4).

Simulation results of half adder and half subtractor are verified successfully using MATLAB, as shown in Fig. 11 , which indicates the proper operation of the device.


Fig. 10. Eye diagram for the sum/difference of half adder and subtractor


Fig. 11. MATLAB results for half adder and subtractor

Half adder and half subtractor are the basic arithmetic unit in the digital system. A full adder circuit can be implemented using two half adders, able to add three bits and produce the sum and carry as output. In this work, the optical cost of the circuit is computed based on the number of MZI elements are used, and delay ( $\Delta$ ) is estimated as
the number of cascaded structures of MZI elements by unit delay $(\Delta)$. Here no other components like beam combiner and beam splitter are used, which are necessary for the SOA-based devices


Fig. 12. Full adder and full subtractor
Table 5. Cost estimation for the proposed adder and subtractor circuit

| Device | No. of <br> MZI | Optical <br> cost | Operational <br> delay |
| :--- | :---: | :---: | :---: |
| Half adder | 3 | 3 | $2 \Delta$ |
| Full adder | 5 | 5 | $3 \Delta$ |
| Half subtractor | 3 | 3 | $2 \Delta$ |
| Full subtractor | 5 | 5 | $3 \Delta$ |
| Parallel adder and | $5 n$ | $5 n$ | $3 n \Delta$ |
| Adder <br> subtractor | $7 n$ | $7 n$ | $3 n \Delta$ |

After a discussion of the full adder and subtractor, a parallel adder and subtractor circuit is proposed. Here twobit adders and subtractors are described (Shown in Fig. 13). Control signal $M$ is the mode selector. If $M=0$, then it will work as an adder circuit, and if $M=1$, then it will work as a subtractor. O-E is optical to electrical signal conversion, consists of a photodiode and amplifier. Here subtraction is performed using 2 's complement method.


Fig. 13. Binary parallel adder subtractor circuit

In Fig. 14, the four-bit binary parallel adder circuit is proposed. The cost estimation for the parallel adder and parallel adder subtractor circuit is given in Table 5. The
comparative optical cost estimation reported by others is given in Table 6.


Fig. 14. Binary parallel adder circuit

Table 6. Optical cost and delay assessment with other reported work

| Ref | Thomsen | Nair et al. | Thapliyal | Kotiyal | Datta | Proposed work |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | et al. [42] | [43] | et al. [44] | $\begin{aligned} & \text { et al. } \\ & \text { [45] } \end{aligned}$ | $\begin{aligned} & \text { et al. } \\ & \text { [41] } \end{aligned}$ | HA | FA | HS | FS | PA |
| Optical cost | $8 n-8$ | $18 n-8$ | $19 n+5$ | $6 n+2$ | $4 n$ | 3 | 5 | 3 | 5 | $5 n$ |
| Delay ( $\boldsymbol{\Delta}$ ) | $3 n+2$ | $4 n+1$ | $4 n+4$ | $3 n+1$ | $2 n$ | 2 | 3 | 2 | 3 | $3 n$ |

## 5. Conclusion

In this paper, the half adder and subtractor, with the help of Mach-Zehnder interferometers-based switch, is realized. Both these circuits are realized using a single circuit. These circuits are elementary for the arithmetic of binary data manipulations and have various applications in optical computing. This paper explains the successful design of the circuit mentioned above using the electrooptic effect of LiNbO3 MZI in BPM and mathematical description. These results are verified using MATLAB simulations. For the proposed device extinction ratio, 38.34 dB has been obtained and much better than the permissible limits.

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## Appendix A1

The detailed simulation process for the proposed design is given below:

Case 1: $A=0, B=0$
An optical signal is applied at the first input port of the MZI AS1. The control signal $A=0$, so the optical signal is obtained at the second output port of the MZI

AS1. This port is connected with the second input port of MZI AS3 and the first input port of MZI AS4. Since control signal $B=0$, the output signal is obtained at the first output port of MZI AS3 and the second output port of the MZI AS4, i.e., $S / D=0, B=0$. The optical power at the first output port of the MZI AS1 is zero, so no signal emerges at the second output port of the MZI AS2, i.e., $C=0$. So the output of the adder is $S / D=0, C=0$ and the result of the subtractor is $S / D=0, B=0$.

Case 2: $A=0, B=1$
As discussed in the previous case, if $A=0$, then an optical signal is obtained at the second output port of the MZI AS1. No power emerged at the second input port of the MZI AS2, so control signal $B=1$ does not make any change at the second output port of the MZI AS2, so $C=0$. Control signal $B=1$, the incoming optical has emerged at the second output port of MZI AS3, and first output port of the MZI AS4, i.e., $S / D=1, B=1$ output of the half subtractor is verified. The output of the half adder is $S / D=1, C=0$.

## Case 3: $A=1, B=0$

The control signal $A=1$, an optical signal is obtained at the first output port of the MZI AS1. The control signal $B=0$, the incoming optical signal is obtained at the first output port of the MZI AS2 (i.e., $C=0$ ) and the second output port of the MZI AS3 $(S / D=1)$. The output of the adder will be $S / D=1, C=0$. The input of the MZI AS4 is zero, so output at the first output port of the will be zero, i.e., $B=0$. The result of the subtractor is $S / D=1, B=$ 0 .

## Case 4: $A=1, B=1$

As discussed in the previous case, $A=1$, an optical signal emerges at the first output port of the MZI AS1. This output port is connected with the second input port of MZI AS2 and the first input port of MZI AS3. Since the control signal $B=1$, the optical signal is obtained at the second output port MZI AS2 and the first output port of the MZI AS3, i.e., $S / D=0, C=1$. The output of the adder circuit is $S / D=0, C=1$. The input of the MZI AS4 is zero, so the result at the first output port of the will be zero, i.e., $B=0$. The result of the subtractor is $S / D=0, B=0$.

Above all, the cases are varied with the truth table Table 2 of the half adder and subtractor.

## Appendix A2

Fig. 13 is the extension of the half adder and subtractor circuit. Fig. 13 is a 2-bit parallel adder and subtractor circuit. The two-bit numbers are $A_{1} A_{0}$ and $B_{1} B_{0}$. When we add parallel


The result will be $C_{1} S_{1} S_{0}$.

Table A1. A truth table for parallel adder and subtractor circuit

| $\mathbf{M}$ | $\boldsymbol{A}_{\mathbf{1}}$ | $\boldsymbol{A}_{\mathbf{0}}$ | $\boldsymbol{B}_{\mathbf{1}}$ | $\boldsymbol{B}_{\mathbf{0}}$ | $\boldsymbol{C}_{\mathbf{1}}$ | $\boldsymbol{S}_{\mathbf{1}}$ | $\boldsymbol{S}_{\mathbf{0}}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Adder |  |  |  |  |  |  |  |
| 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 0 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| Subtractor |  |  |  |  |  |  |  |
| 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 0 | 1 | 1 | 1 | 1 | 1 | 0 | 0 |

Fig. A2.1 shows the binary parallel adder and subtractor circuit with addition operation, and Fig. A2.2 shows the binary parallel adder and subtractor with subtraction operation. Two cases are verified using the beam propagation method and given for your reference. Similar other cases can be realized. Table A1 consists of the truth table for the binary parallel adder and subtractor circuit.

Fig. A2.1: Binary parallel adder and subtractor (addition operation) (color online)

Fig. A2.2: Binary parallel adder and subtractor (subtraction operation) (color online)


In Fig. A2.3, the two-bit binary parallel circuit is designed. Two cases are simulated using BPM. Similarly, cases can be realized using the proposed design. Further, a four-bit parallel adder circuit can be implemented. Table A2 shows the truth table for the parallel adder circuit.

Table A2: Truth table for parallel adder

| $A_{1}$ | $A_{0}$ | $B_{1}$ | $B_{0}$ | $C_{1}$ | $S_{1}$ | $S_{0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 1 | 1 | 1 | 1 | 1 | 1 | 0 |



Fig. A2.3: 2 Bit parallel adder (color online)

